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- 1) IEC and Helicon
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IEC:



- IEC at UIUC modified into a space thruster.
- IEC has several modes. The mode that is shown here is "jet" mode.

Helicon:



- A type of RF discharge in the presence of an axial magnetic field.
- Helicons are a high density plasma source (10¹⁷ m⁻³ – 10¹⁸ m⁻³).

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What is HIIPER?



Helicon Injected Inertial Plasma Electrostatic Rocket (HIIPER)

Helicon plasma injected IEC combination

What is HIIPER?

HIIPER Configuration



Representative model of the HIIPER



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Analysis of Helicon

Distribution of power to the different reactions in a <u>helicon plasma</u>



Analysis of Helicon

Lessons from the analysis:

- Minimize surface area of the dielectric tube without minimizing plasma volume.
- Decrease height of cylinder and increase radius.

$$S = 2\pi r H$$
$$V = \pi r^2 H$$

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Model of the IEC-Helicon interface similar to a DC plasma sheath.

Description of the model:

- The "bulk plasma" region is in the helicon.
- The sheath region is in the IEC.

Schematic model of the Helicon-IEC interface



Ion flux approximated by the following equation:

$$\Gamma_i = \mu_i n_i E - D_a \nabla n_i$$

μ_i: ion mobility
 n_i: ion number density
 D_a: ambipolar diffusion coefficient
 E: electric field

(Chen, 2006)

$$\Gamma_i = \mu_i n_i E - D_a \nabla n_i$$

How do we find the variables to this equation?



(Lieberman, 2005)

Conditions in the sheath vary drastically. For example:

- quasi-neutrality does not hold
- most of the voltage drop occurs in the sheath



Conditions to determine the variables in the ion flux equation are less erratic in the presheath.

The different properties of the presheath can be determined from various diagnostics, for example:

Langmuir Probe:

- Electron temperature in the helicon
 - Electron density in the helicon

Emissive Probe:

Length of the presheath

Spherical Langmuir Probe



Calculation from the model previously described compared with experiment:

- Spherical probe used to mimic the potential profile of the spherical IEC grid
- Spherical probe biased to -3000 V, this would put the probe in the ion saturation region
- Ion current collected at a specific voltage bias

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The geometry of the helicon dielectric tube plays an important role in plasma formation efficiency which affects flow rate

- Shorter length
- Larger radius

Presheath measurements can be used to estimate the ion flow from the helicon to the IEC.

 Plasma density and electron temperature in the bulk plasma can be determine from a RF-compensated Langmuir probe

$$\Gamma_i = \mu_i n_i E - D_a \nabla n_i$$

 Density drop in the presheath can be determined from the Boltzmann relation

Boltzmann Relation: $n(V) = n_0 e^{\frac{e(V-V_0)}{T_e}}$

- Voltage drop in presheath on the order of the electron temperature in eV divided by elementary charge
- Length of the presheath determine by emissive probe

$$\Gamma_i = \mu_i n_i E - D_a V n_i$$

Mobility and ambipolar diffusion coefficient can be determine from:

- The ion temperature (approximately equal to the neutral gas temperature)
- Neutral gas density (from pressure)
- Mean free path of neutral gas atoms (given the temperature range it can approximated as hard sphere collision)
- Electron-ion collision frequency (given in (Chen, 2006))

$$\Gamma_i = \mu_i n_i E - D_a \nabla n_i$$

| RF FWD: (W) | Calculated Ion Flow Rate: (s ⁻¹) | Measured Ion Flow Rate: (s ⁻¹) | Error (%) | Normalized Error |
|-------------------|--|--|--------------|---------------------|
| 30 | 9.37×10 ¹⁵ | 1.78×10 ¹⁶ | 47 | 0 |
| 60 | 1.27×10 ¹⁶ | 2.70×10 ¹⁶ | 53 | -0.13 |
| 90 | 1.46×10 ¹⁶ | 3.54×10 ¹⁶ | 59 | -0.26 |
| 120 | 1.70×10^{16} | 4.21×10 ¹⁶ | 60 | -0.28 |
| 150 | 1.87×10 ¹⁶ | 4.77×10 ¹⁶ | 61 | -0.30 |
| 180 | 1.99×10 ¹⁶ | 5.39×10 ¹⁶ | 63 | -0.34 |
| 210 | 2.14×10 ¹⁶ | 5.85×10 ¹⁶ | 63 | -0.34 |
| 240 | 2.32×10 ¹⁶ | 6.28×10 ¹⁶ | 63 | -0.34 |
| 270 | 2.37×10 ¹⁶ | 6.83×10 ¹⁶ | 65 | -0.38 |
| 300 | 2.67×10 ¹⁶ | 6.86×10 ¹⁶ | 61 | -0.30 |

Calculation are based on experimental measurement (e.g. Langmuir probe) and several approximations

Agreement between experimental and calculated results are thought to be reasonable given errors associated with many theoretical and experimental comparison for plasmas.

The present measurement shows that the ion flow rate can be increased by shortening the presheath length by decreasing the helicon tube length and the distance of the high density plasma in the helicon from the IEC.

The goal of the improved flow rate into the IEC can be achieved by careful design of the helicon geometry combined with the optimization of the helicon-IEC coupling region.

Future Work

Calculations were determined from previous experimental data and information

Perform new diagnostic measurement (e.g. emissive probe measurements) such as mapping the potential profile from the helicon into the IEC to reconfirm results

Consider a inverted helicon design to increase ion density and hence flow rate to the IEC (Masters, 2010).

Acknowledgment

- NPL Associates
- Air Force Research Lab
- National Systems
- NASA

Works Cited:

M. N. Lieberman and A. J. Lichtenberg, Principles of plasma discharges and materials processing, Hoboken, NJ: John Wiley & Sons, Inc, 2005.

F. F. Chen, Introduction to plasma physics and controlled fusion, New York: Plenum Press, 2006.

Works Cited:

G. Chen, "Analysis of Energy Balance in a Helicon
Coupled to an Inertial Electrostatic Confinement Device,"
University of Illinois at Urbana-Champaign, Urbana,
2013.

B. C. Masters, "Development and Characterization of Conventional and Inverted Helicon Plasma Sources," University of Illinois at Urbana-Champaign, Urbana, 2007.

| Conc | | RF Calculated Ion FWD: Flow Rate: | | Measured Ion Flow Rate: | Error (%) | Error Normalized (%) Error | | |
|------|---------------------------|---|---------------------------|--------------------------------|-------------------|-------------------------------|-------------|--|
| RF | Calculated Ion | (** <i>)</i> Micagui cu ion | (5) | | | | | |
| FWD: | Flow Rate: | Flow Rate: | (%) | Error | 47 Ca | culation a | re based on | |
| (W) | (s ⁻¹) | (s ⁻¹) | | | ⁵³ exr | erimental | | |
| 30 | 9.37×10 ¹⁵ | ⁹ 9.78×10 ¹⁶ ^{1.4} | 46×10^{16} 47 | 3.54×10^{16} | 59mo | | | |
| 60 | 1.27×10 ¹⁶ | 120.70×10 ¹⁶ 1.7 | 70×10 ¹⁶ 53 | 4.21×10^{16} -0.13 | | -0,28 | | |
| 90 | 1.46×10 ¹⁶ | 159.54×10 ¹⁶ 1.8 | 37×10 ¹⁶ 59 | 4.77×10 ¹⁶ -0.26 | Lar | ngmuir pro | be) and | |
| 120 | 1.70×10 ¹⁶ | 180.21×10 ¹⁶ 1.9 | 99×10 ¹⁶ 60 | 5.39×10 ¹⁶ -0.28 | ₆₃ sev | /eral_ <u>a</u> ppro | ximations | |
| 150 | 1.87×10 ¹⁶ | 214.77×10 ¹⁶ 2.1 | 14×10 ¹⁶ 61 | 5.85×10 ¹⁶ -0.30 | 63 | -0.34 | | |
| 180 | 1.99×10 ¹⁶ | 249.39×10 ¹⁶ 2.3 | 32×10 ¹⁶ 63 | 6.28×10 ¹⁶ -0.34 | 63 | -0.34 | | |
| 210 | 2.14×10 ¹⁶ | 279.85×10 ¹⁶ 2.3 | 37×10 ¹⁶ 63 | 6.83×10 ¹⁶ -0.34 | 65 | -0.38 | | |
| 240 | 2.32×10 ¹⁶ | 300.28×10 ¹⁶ 2.6 | 63 57×10 ¹⁶ | 6.86×10 ¹⁶ -0.34 | 61 | -0.30 | | |
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